



Robert
Bird
Group

Basis of Design Report
Early Works (Shoring) Package
Liverpool Civic Place

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Appendix A RBG Early Works (Shoring) Package Drawings

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1.0 Introduction

This **RBG Basis of Design Report – Early Works (Shoring) Package** is submitted to Liverpool City Council (Council) in support of a Development Application (DA) for site preparation and early works at 52 Scott Street, Liverpool (the site) also known as the Liverpool Civic Place site. Specifically, the DA seeks approval for:

- Demolition of all existing structures and site improvements; and
- Bulk earth works to a depth of **RL10.35** including shoring through the use of piles.

The proposal relates to the broader Liverpool Civic Place site redevelopment plan which is detailed within the Concept DA (DA/485/2019) submitted to Council on 17 September 2019. Specifically, the Concept Proposal seeks approval for various uses within proposed building envelopes, including:

- A building envelope with a maximum height of RL 43.45 for the purpose of an information and education facility (public library) use.
- A building envelope with a maximum height of RL 84.25 for the purpose of a public administration building use, and either (or a combination of) commercial premises or child-care centre uses.
- A building envelope with a maximum height of RL 118.85 which will accommodate either (or a combination of) commercial premises, educational establishments, tourist and visitor accommodation or boarding house (student accommodation) uses.
- A landscaping and public domain concept including the provision of a public through-site link running north to south through the site, connecting Scott Street to the north through to Terminus Street to the south; and
- A building envelope for a three-level shared basement car park across the entire site to accommodate parking for all future uses (approximately 413 spaces, to be determined as part of future detailed DAs) and accommodating a public car park to be owned by Council.

The detailed design of the Liverpool Civic Place will be subject of separate Stage 2 DA(s). The benefits of this approach would allow the expedited local assessment and determination of an application for these additional 'early works', which are key to ensuring the development can be delivered in a timely manner.

2.0 Scope and Limitations

The purpose of this report is to outline the design assumptions and requirements adopted by RBG for the structural design of the retention system and provide the structural scheme design/advice for the Early Works Development Application (DA) Submission. Note this is intended to provide basis of design for review by the design team. It does not supersede the project design brief and specifications that should be referred to for all general assumptions and requirements.

Furthermore, it should be stated that at this point of time, the design has been developed to the level of a preliminary design only. Further information and analysis are required to be confirmed with Built.

3.0 Reference Documents

- FJMT Architectural Drawings dated 13th August 2019, Rev E
- RBG Structural Design Sketches
- Golder Geotechnical and Environmental Investigation Report dated 22 August 2019, Rev 0
- Golder Preliminary Geotechnical Assessment Report, Reference No. 19125312-002-L-Rev0 dated 15 November 2019

4.0 Geotechnical Conditions

Refer to “*Golder Geotechnical and Environmental Investigation Report*” referenced in Section 2 for site geotechnical conditions and constraints. RBG notes that further geotechnical analysis and design may be required as the project progresses.

Below is a summary of our understanding:

4.1 Groundwater

In accordance with the “*Golder Preliminary Geotechnical Assessment Report*”, the groundwater level measured in August 2019 is generally at RL +17.5 m AHD, approximately 7.0 m higher than the proposed bulk excavation level (BEL) at RL +10.35 m AHD.

4.2 Proposed Retention System

A drained basement has been identified as applicable for this development and is the basis of structural design, as confirmed by the client.

Consequently, Golder have recommended to use a retention system consisting of anchored soldier piles with shotcrete infill walls and vertical cuts in the underlying competent rock (i.e. Unit 3b and 4). It has been also suggested to use pattern bolting and shotcrete facing for Unit 3a.

Golder have also recommended to control the seepage into the excavation during construction and in the long-term case by perimeter and subfloor drainage connecting into a pump and sump system for a drained basement.

5.0 Design Criteria

5.1 Stage of Design

The proposed design is preliminary only and may subject to change upon review.

5.2 Bulk Excavation

RBG have understood that the development consists of a three-level basement carpark and a bulk excavation level (BEL) to RL +10.35 m AHD. This has been a direction from the client team and identified by the masterplan DA submission. Refer to Figure 1 for a section of the masterplan envelope.

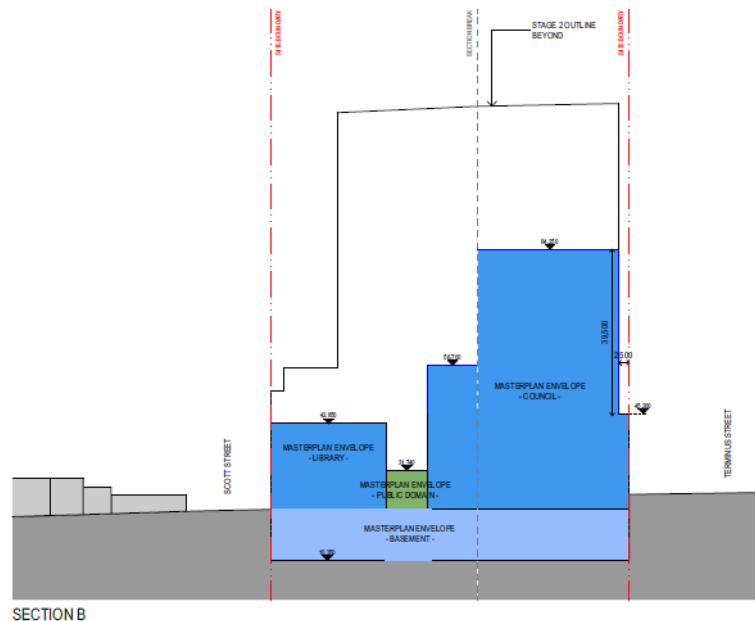


Figure 1 - Masterplan Envelope - Section A

The existing ground level along the southern part of the site (along the Terminus Street) is approximately at RL +26 m AHD, about 3 m higher than the ground level along the northern part of the site (along the Scott Street).

5.3 Excavation Staging

RBG is understood that two bulk excavation options are considered by Built at this stage, including: Option 1 – bulk excavation for the whole development; Option 2- dividing the bulk excavation into two stages. The two-stage excavation process will include excavation under the library and council buildings as part of Stage 1, and excavation under the commercial and hotel buildings as part of Stage 2.

If the two-stage excavation is considered, Stage 1 and 2 can be separated by battering the soil towards stage 2 as per the requirements specified by geotechnical engineer (Option 2). Should a two-stage excavation option commence, the supporting structure for the buildings above and dividing wall between the stages will be documented in the detailed DA submission for the proposed building/s.

5.4 Retention System

- As a drained basement option is considered, temporary drainage would need to be provided during construction to manage estimated water inflows. Water would need to be managed from excavation walls and an allowance shall be made for pumping and disposal of this water.
- Current design is based on the results from two analysis sections adopted by Golder and presented in “Golder Preliminary Geotechnical Assessment Report”. Refer to Figure 2 for the layout of these analysis sections.

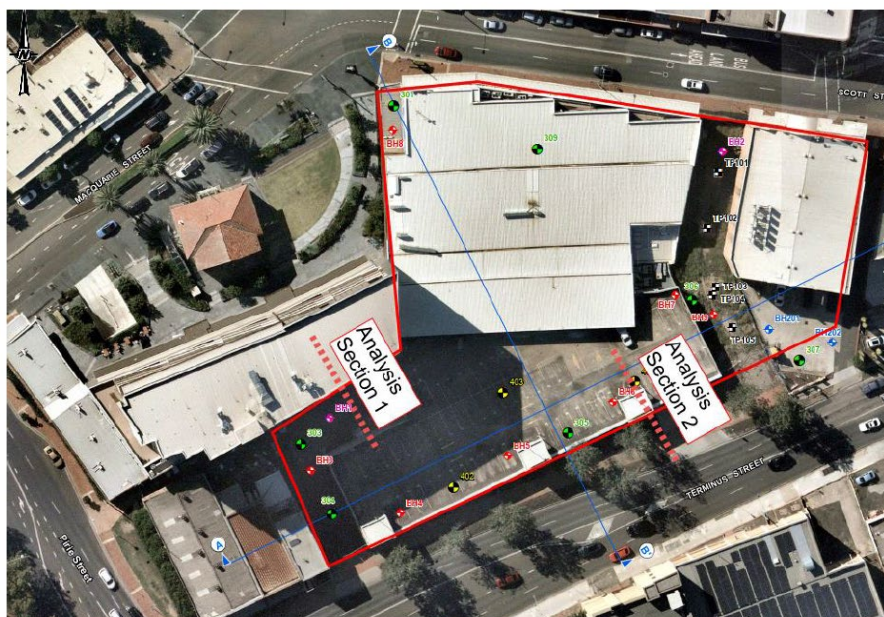


Figure 2 – Geotechnical Analysis Section layout adopted by Golder

- No long-term loadings from vertical structural elements are considered to load the retention system. This has been a direction from the client team.
- All ground anchors are assumed to provide temporary support only and be destressed as the construction of basement floor slabs progresses.
- In the permanent condition, the floor slabs of the basement structure are assumed to provide lateral support to the retention system.
- The foundation loads from Matchworks building (adjacent building to Analysis Section 1) are considered as an equivalent strip load. They are presented in Section 5.6.3.3. This design assumption has also been discussed with the Geotechnical Engineers at a design meeting hold on 5th November 2019.
- The maximum displacement of the retention walls is limited to 10 mm for sections adjacent to Matchworks building and to 15 mm for typical sections.
- As recommended by Golder, soldier piles of the retention system adjacent to Matchworks building are extended to have a socket of 0.5 m in Unit 4. In addition, an allowance for rock bolts at 0.5 m below the pile toe is made.
- Soldier piles of the typical retention system are extended to have a socket of 0.5 m in Unit 3a.
- As identified by Golder, soldier piles do not need to be extended to RL below BEL and can stop short, approximately, at the RLs specified on RBG Early Works (Shoring) Package Drawings. These RLs to be finalised/confirmed by geotechnical engineers following more detailed design and analysis in the next stage. Furthermore, having a rock face with rock bolting as required is an acceptable retention solution by Golder.
- Where the rock facing is considered as the retention system, further columns/walls are required to support basement slabs and beams.

5.5 Design Standards and Guidelines

The structural design for the proposed retention system is in accordance with the current revision of all relevant Australian/New Zealand Standards. These standards will include, but are not limited to:

- **AS/NZS 1170.0: 2002:** Structural design actions – Part 0: General principles
- **AS/NZS 1170.1:2002:** Structural design actions – Part 1: Permanent, imposed and other actions
- **AS 3600:2009:** Concrete structures
- **AS/NZS 4671:2001:** Steel reinforcing materials
- **AS 4678:2002:** Earth-retaining structures

5.6 Design Input Information

5.6.1 Design Parameters for Ground Unit

The geotechnical parameters adopted in this design are based on what have been provided in “*Golder Preliminary Geotechnical Assessment Report*”.

Table 1. Design parameters for ground units

Ground Unit	γ (kN/m ³)	C' (kPa)	ϕ' (°)	E_{50} (MPa)	E_{ur} (MPa)	K_o (-)
Unit 1 Filling	17	0	30	10	20	0.5
Unit 2 St-H Residual clay	18	5	28	20	40	1
Unit 3a L-M Laminite	24	50	38	200	400	1
Unit 3b M-H Laminite	24	200	40	1,200	2,400	2 ¹
Unit 4 H-VH Sandstone	24	400	43	2,000	4,000	6 ¹

¹ – K_o is elevated to generate the estimated locked-in horizontal stress

Source: Golder

5.6.2 Material Properties for Structural Elements

Unless noted otherwise, the following minimum values will be used for material properties:

- Material density:
 - Concrete: 24.5 kN/m³
 - Steel: 76.9 kN/m³
- Material strength:
 - Concrete – piles, capping beam, shotcrete: $f'_c = 40$ MPa
 - Reinforcement: $f_{sy} = 500$ MPa
- Modulus of Elasticity (based on 28 days concrete strength):
 - Concrete – piles, capping beam, shotcrete: 32,800 MPa
 - Reinforcement: 200,000 MPa

5.6.3 Design Loads

Refer to RBG Early Works (Shoring) Package Drawings – ST-01150 [P1] for shoring loading plan. The design loads considered are briefly discussed in the following:

5.6.3.1 Dead Loads

The dead loads considered in the design of retention system are calculated from self-weight and super-imposed dead load from the upper structure. Dead loads are assumed to be applied on the capping beam as a line load.

5.6.3.2 Live Loads

The live loads considered in the design of retention system are calculated from the imposed live load from the ground floor slab. Live loads are assumed to be applied on the capping beam as a line load.



5.6.3.3 Surcharge Loads

- Scott Street: 20kPa
- Just Sport – Liverpool: 15kPa
- Terminus Street: 20 kPa
- The Window Tinting Centre: 15 kPa
- Match works Building:
 - 355kN/m line load on neighbouring building capping beam
 - 650kPa surcharge under the 1st row of neighbouring building columns
 - 470kPa surcharge under the 2nd row of neighbouring building columns

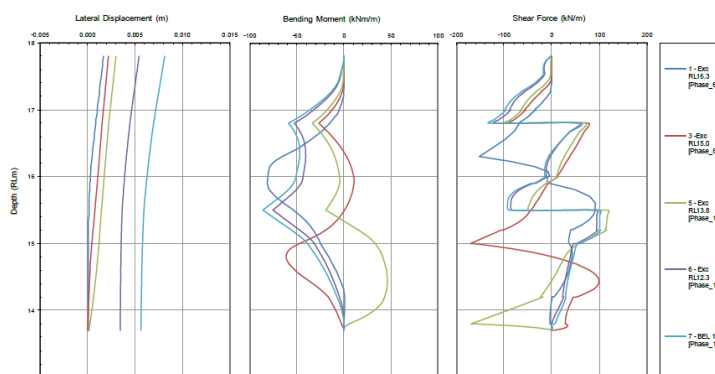
5.6.3.4 Earth Pressure

A lateral pressure of 20 kPa is adopted for designing the shotcrete walls as suggested by Golder.

5.6.3.5 Forces in Soldier Piles

Analysis Section 1 – Adjacent to Matchworks Building

600 diameter soldier piles at 1.5 m spacing have been considered. The design forces computed for Analysis Section 1, according to Golder report, are as follows:



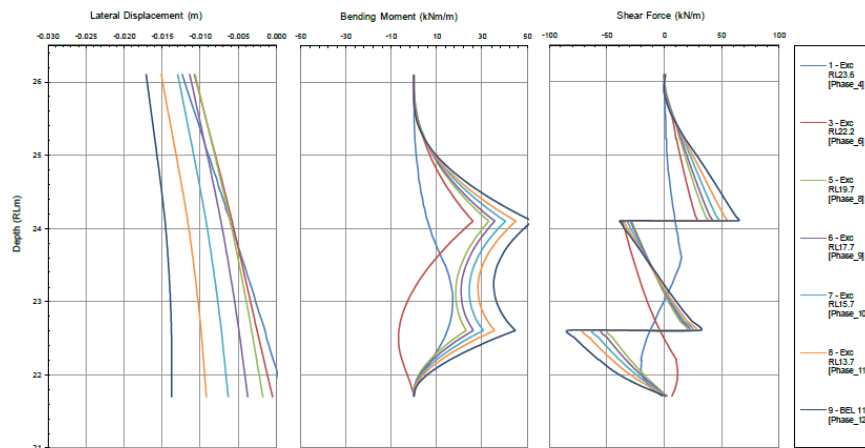
Construction Stage	Wall Lateral Displacement (mm)	Maximum Bending Moment ¹ (kNm)	Maximum Shear Force ¹ (kN)
Excavate to RL16.3	2	122	229
Excavate to RL15.0	2	91	256
Excavate to RL13.8	3	69	254
Excavate to RL12.3	5	113	183
Excavate to RL10.35	8	132	202

Source: Golder

Figure 3 – Lateral displacement and forces induced in the proposed soldier pile wall (adjacent to Matchworks Building)

Analysis Section 2 – Typical Section

600 diameter soldier piles at 2.4 m spacing have been considered. According to Golder report, the design forces computed for Analysis Section 2 are as follows:



Construction Stage	Wall Lateral Displacement (mm)	Maximum Bending Moment ¹ (kNm)	Maximum Shear Force ¹ (kN)
Excavate to RL23.6	13	41	49
Excavate to RL22.2	11	62	88
Excavate to RL19.7	11	79	118
Excavate to RL17.7	11	86	131
Excavate to RL15.7	13	97	150
Excavate to RL13.7	15	108	170
Excavate to RL10.35	18	126	207

Source: Golder

Figure 4 – Lateral displacement and forces induced in the proposed soldier pile wall (typical section).

5.6.3.6 Forces in Temporary Anchors

Analysis Section 1 – Adjacent to Matchworks Building

According to Golder report, the design parameters considered for temporary anchors of Analysis Section 1 are as follows:

Table 2. Design parameters considered for temporary anchors of Analysis Section 1.

Row	Spacing (m)	Inclination (°)	Anchor Prestress Load ¹ (kN/anchor)	Maximum Axial Force ¹ (kN/anchor)
R1	1.5	15	250	350
R2	1.5	15	250	300

¹ – Value shown is unfactored and a waler is required to distribute the load equally in a row.

Source: Golder

In addition, a minimum anchor free-length of 4.0 m is considered.

Analysis Section 2 – Typical Sections

According to Golder report, the design parameters considered for temporary anchors of Analysis Section 2 are as follows:

Row	Spacing (m)	Inclination (°)	Anchor Prestress Load ¹ (kN/anchor)	Maximum Axial Force ¹ (kN/anchor)
R1	2.4	15	150	250
R2	2.4	15	150	300

¹ – Value shown is unfactored.

Source: Golder

In addition, the anchor fixed-length should be located beyond a plane projected at an angle of 45 degrees from horizontal from the base of Unit 3a.

5.6.3.7 Design Load Combination

Ultimate Limit State:

- 1.35 G (total)
- 1.2 G (total) + 1.5 Q (total)

Serviceability Limit State:

- G (SW) + G (SDL) + 0.4Q (total) + H (LT, service)

5.6.3.8 Durability and Crack Control Methodology

- Design life = 50 years
- Concrete grade = 40MPa
- Concrete cover:
 - Piles = 65mm
 - Capping beam = 50mm
 - Shotcrete - retained soil side = 65mm
 - Shotcrete – excavation side = 30mm
- Crack width limit = moderate crack control as required by AS 3600:2009

5.7 Temporary Batter Slop Between Construction Stage 1 and Stage 2

Refer to “Golder Preliminary Geotechnical Assessment Report” referenced in Section 2 for temporary batter slopes may be adopted between Stage 1 and 2.

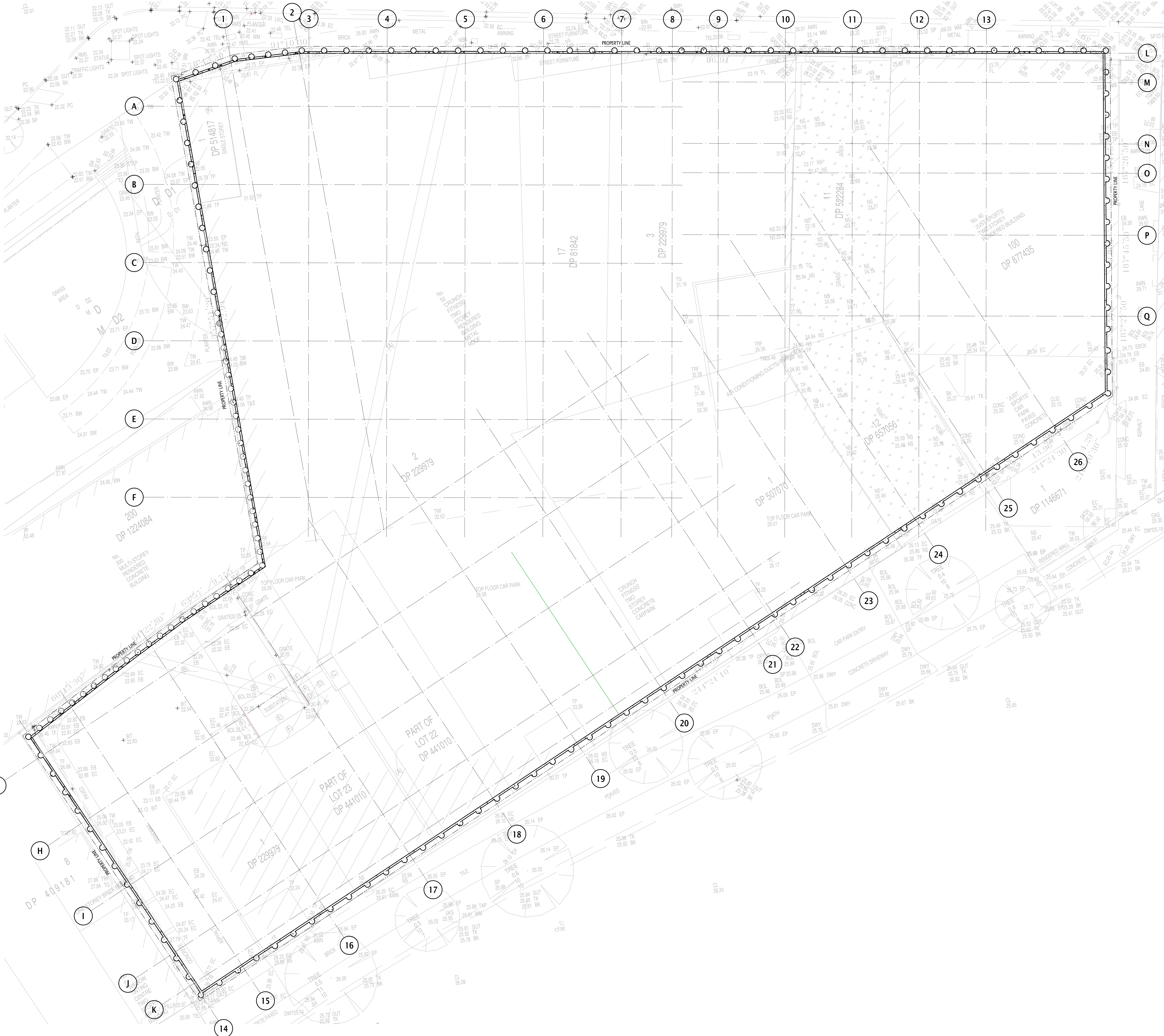
6.0 Conclusion

During Early Works DA design development, RBG have provided advice and input into the design of retention system (early works shoring package) by producing preliminary structural drawings (Appendix A) for the design team to incorporate into the design and attending weekly design coordination meetings.

Appendix A

RBG Early Works (Shoring) Package Drawings





SHORING SURVEY PLAN
SCALE 1:150

NOTES:
- SURVEY OVERLAY AS PER VERIS AUSTRALIA PTY LTD
SURVEY PLAN ISSUED 06.09.2019

P1 EARLY WORKS INFORMATION (ONLY)										ST	CA	25.11.19
Rev	Revision Description	By	App	Date								
0001	1	1	1	1								

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Client
BUILT PTY LTD

Project
LIVERPOOL CIVIC PLACE

Title
SHORING SURVEY PLAN

Date
01.11.19
Scale at 40
1:150

Drawn
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Designer
M.MOCHADDA
Design Checker
G.ANDRIANAKOS

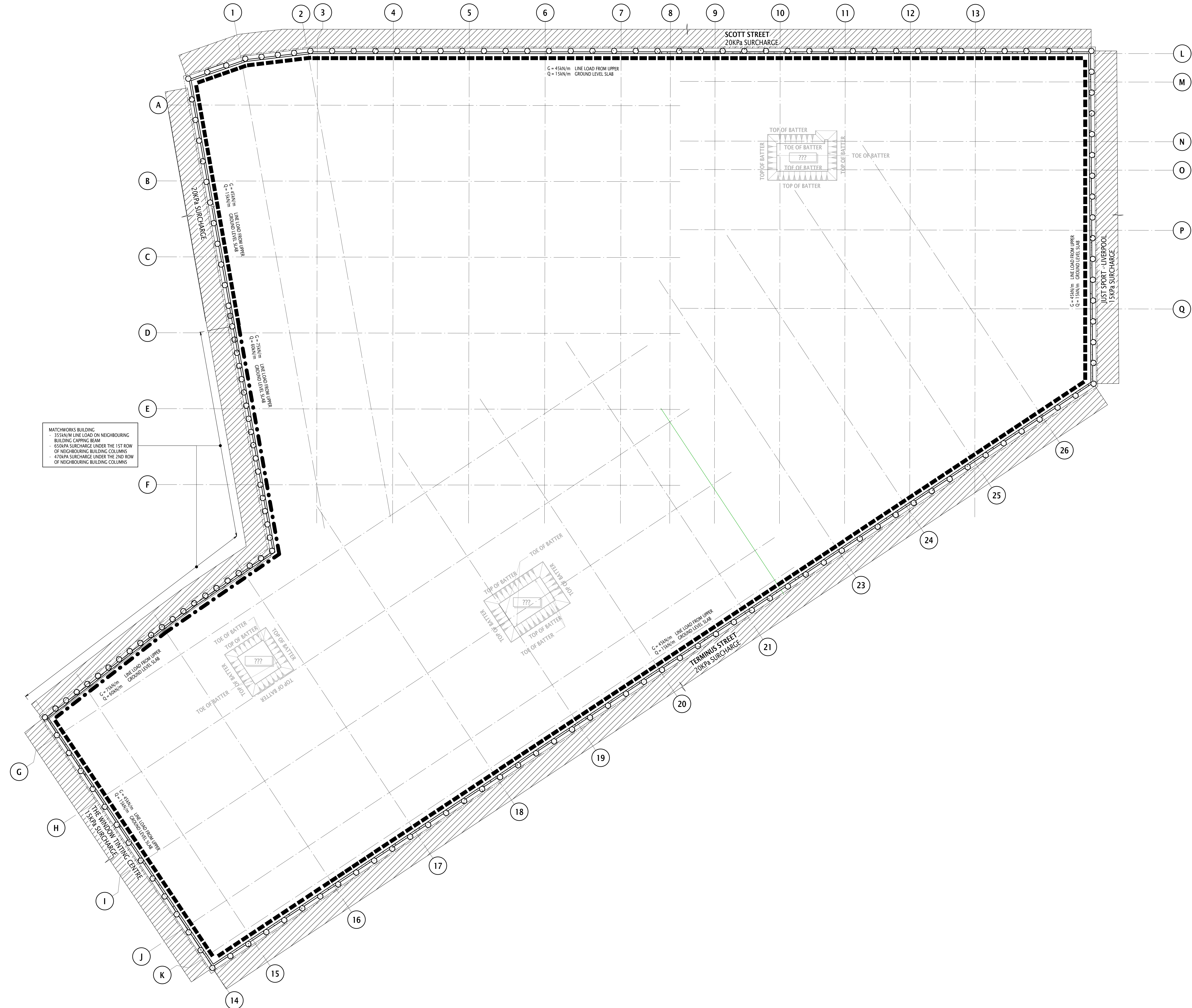
Job Number
19280

Approved
G.ANDRIANAKOS

NOT FOR CONSTRUCTION

Drawing Number
RBG-XX-XX-DR-ST-01010

Revision
P1



SHORING LOADING PLAN
SCALE 1 : 150

NOTES :

1. NO LONG TERM LOADING FROM VERTICAL STRUCTURAL ELEMENTS ARE CONSIDERED TO LOAD THE RETENTION SYSTEM. THIS HAS BEEN A DIRECTION FROM THE CLIENT TEAM
2. THE FOUNDATION LOADS FROM MATCHWORKS BUILDING HAVE BEEN DISCUSSED WITH THE GEOTECHNICAL ENGINEERS AT A DESIGN MEETING HELD ON THE 30th NOVEMBER 2019

LEGEND :

--- DENOTES SURCHARGE LOAD (kPa)

--- DENOTES LINE LOAD (kN/m)

P1 EARLY WORKS (INFORMATION ONLY) ST CA 25.11.19

Rev	Revision Description	By	App	Date
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LIVERPOOL CIVIC PLACE

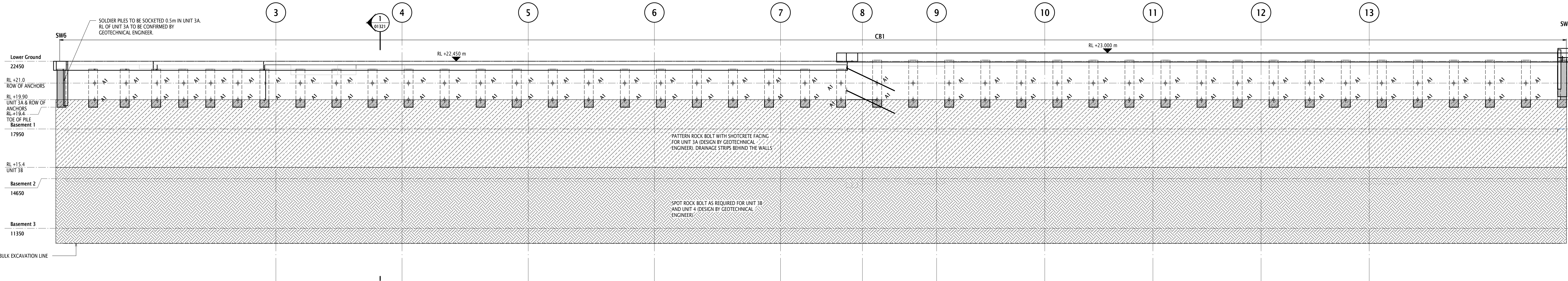
Title
SHORING LOADING PLAN

Date 01.11.19 Scale as 40 1:150	Drawn S.TRIMARCHI Designer M.MOGHADDASSI Design Checker G.ANDRIANAKOS
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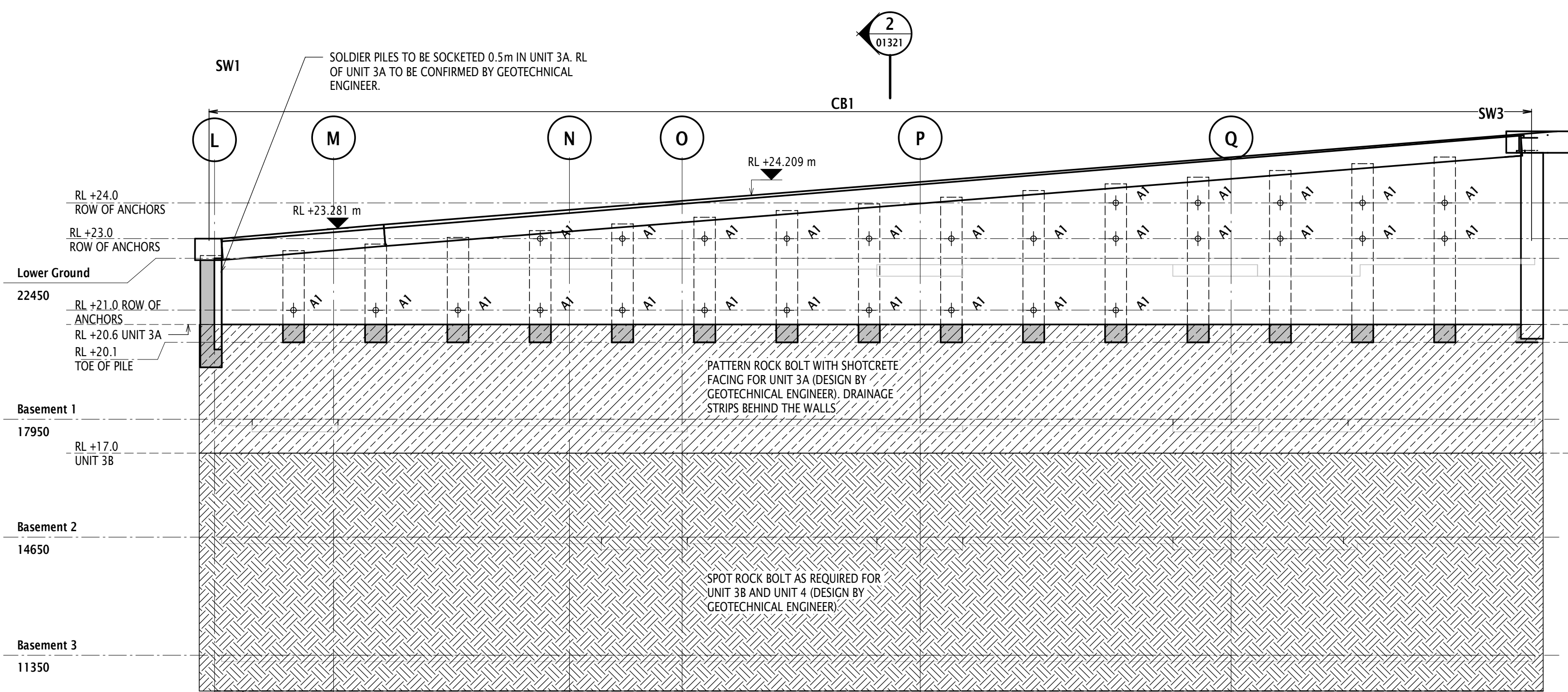
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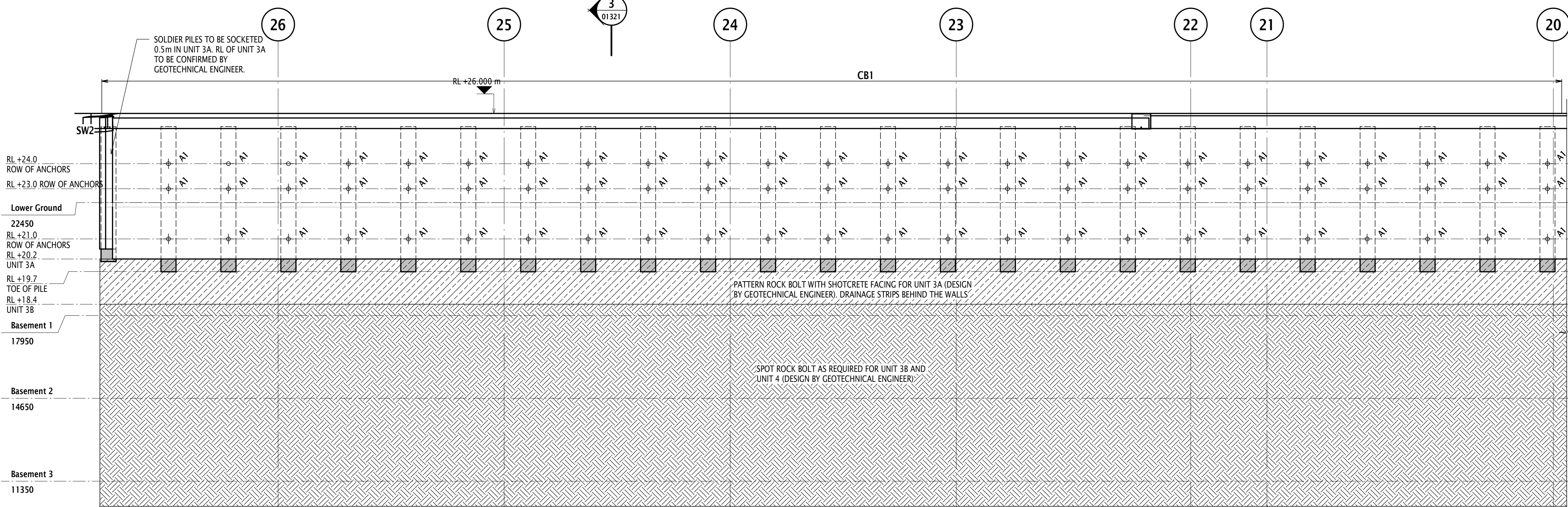
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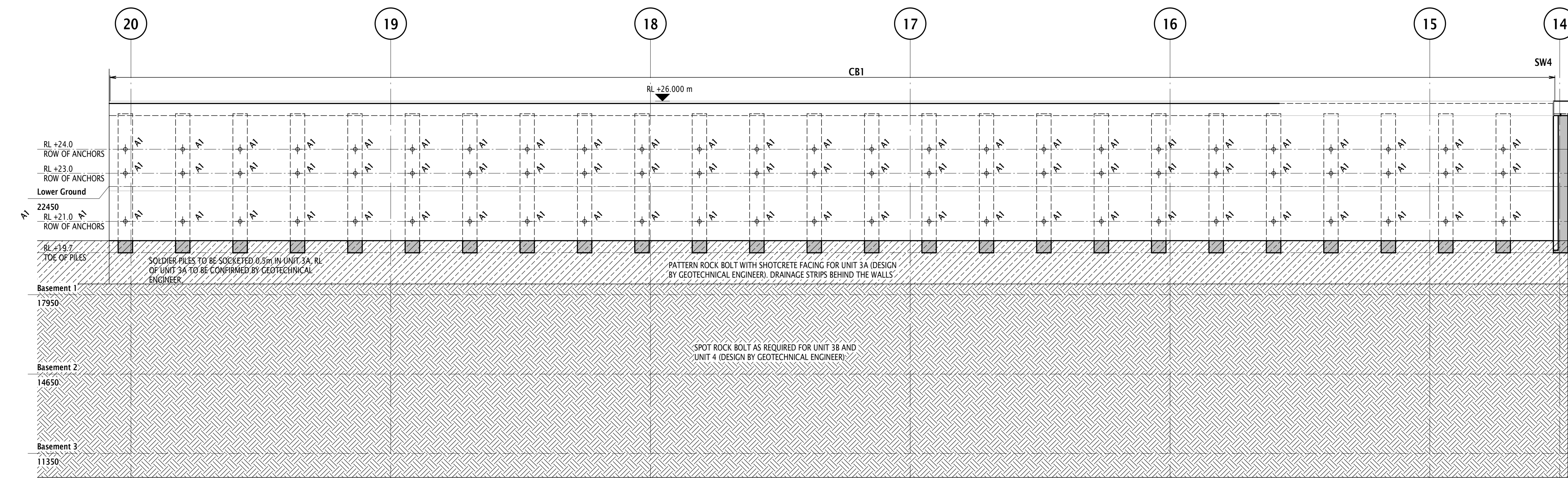
SHORING WALL ELEVATION - SW1
SCALE 1 : 100



SHORING WALL ELEVATION - SW2
SCALE 1 : 100



SHORING WALL ELEVATION - SW3
SCALE 1 : 100



SHORING WALL ELEVATION - SW4
SCALE 1 : 100

- EXCAVATION NOTES:**
- LOCAL EXCAVATION FOR COLUMNS, PILE CAPS, AND STRIP FOOTINGS NOT SHOWN.
 - EXCAVATION SEQUENCE AND REQUIREMENTS TO BE CONFIRMED BY GEOTECHNICAL ENGINEER.
 - GEOTECHNICAL ENGINEER TO INSPECT EXCAVATION.
 - INSPECTION PLAN TO BE CONFIRMED BY GEOTECHNICAL ENGINEER.
- CONCRETE NOTES:**
REFER NOTES ON COVER SHEET
MIN CONC. STRENGTH AT 28 DAYS

LOCATION	Fc
SHOTCRETE	40MPa
BORED PIER	40MPa
CAPPING BEAM	40MPa

CONCRETE COVER	COVER
BORED PIER	65mm
CAPPING BEAM	50mm
SHOTCRETE	50mm
RETAINED SOIL SIDE	65mm
EXCAVATION SIDE	30mm

P1 EARLY WORKS (INFORMATION ONLY) ST CA 25.11.19

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Client
BUILT PTY LTD

Project
LIVERPOOL CIVIC PLACE

Title
**SHORING WALL ELEVATIONS
SHEET 1**

Date
01.11.19
Scale: as 40
1:100

Drawn
S.TRIMARCHI
Designer
M.MOGHADDASSI
Design Checker
G.ANDRIANAKOS

Job Number
19280

Approved
G.ANDRIANAKOS

NOT FOR CONSTRUCTION

Drawing Number
RBG-XX-XX-DR-ST-01211

Revision
P1

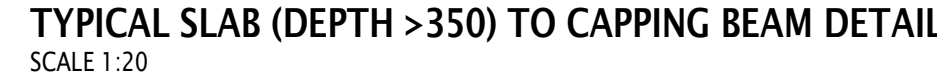
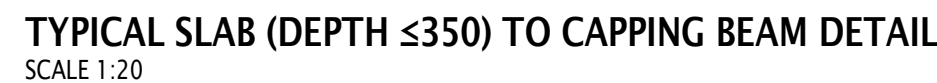
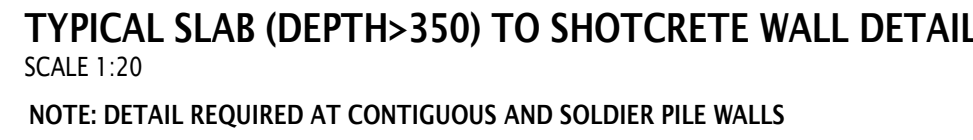
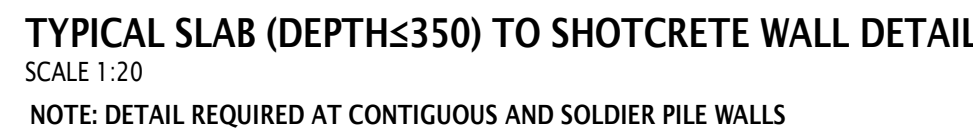
CAPPING BEAM SCHEDULE					
MARK	BREADTH	HEIGHT	TOP & BTM REINFORCEMENT	SIDE REINFORCEMENT	LIGATURES
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CB2	750	600	3N20	4N24	4 LEC3 N12-300

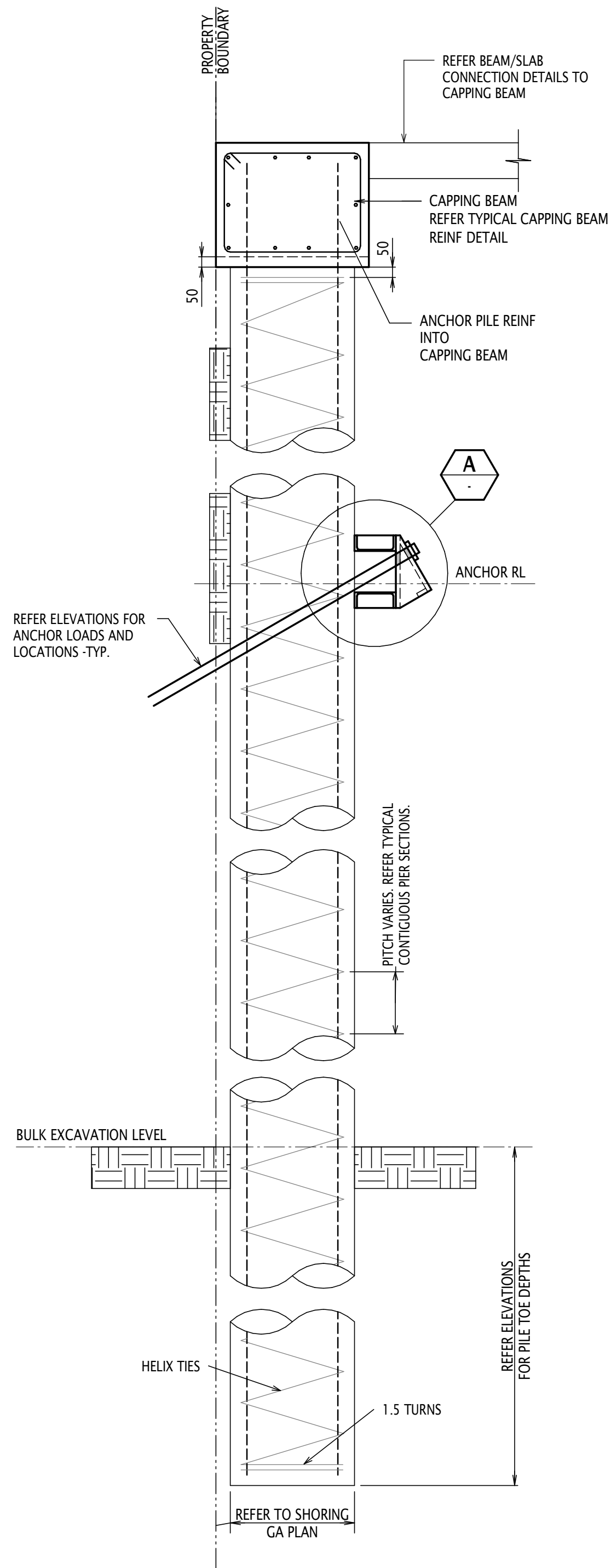
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MARK	DIA	VERTICAL	HELIX TIES	COMMENTS
BP1	600	12N20	N12-300	
BP2	600	12N20	N16-300	

SHOTCRETE WALL SCHEDULE			
THICKNESS	HORIZONTAL	VERTICALS	Comments
200	SL102 MESH EF		

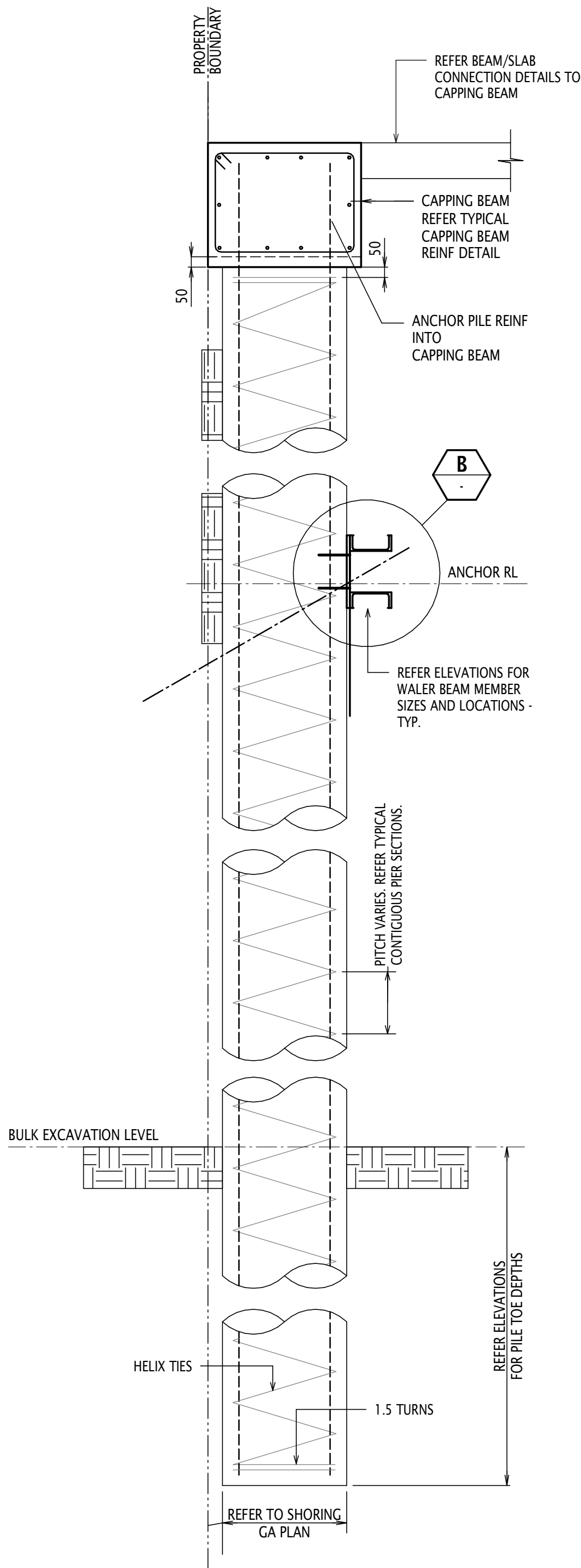
ANCHOR SCHEDULE								
MARK	SAFE WORKING LOAD (kN)	ANGLE FROM HORIZONTAL	DIAMETER (mm)	NO OF STRANDS	MIN.FREE LENGTH (mm)	INDICATIVE BOND IN SHALE/LAMINATE (m)	INDICATIVE TOTAL ANCHOR LENGTH ROCK (m)	PRE-STRESS LOAD (kN)
A1	300	15	100	2				150
A2	450	15	100	3				250

- NOTES:**
- NUMBER OF STRANDS ARE BASED ON 15.2mm SUPER-STRANDS
 - LOW PRE-STRESS LOADS ARE RECOMMENDED TO NOT INDUCE EXCESSIVE BENDING MOMENT AND SHEAR IN THE PILES
 - ANCHOR DETAILS IN ACCORDANCE WITH GOLDER ASSOCIATES SHORING WALL GEOTECHNICAL REPORT DATED NOVEMBER 2019

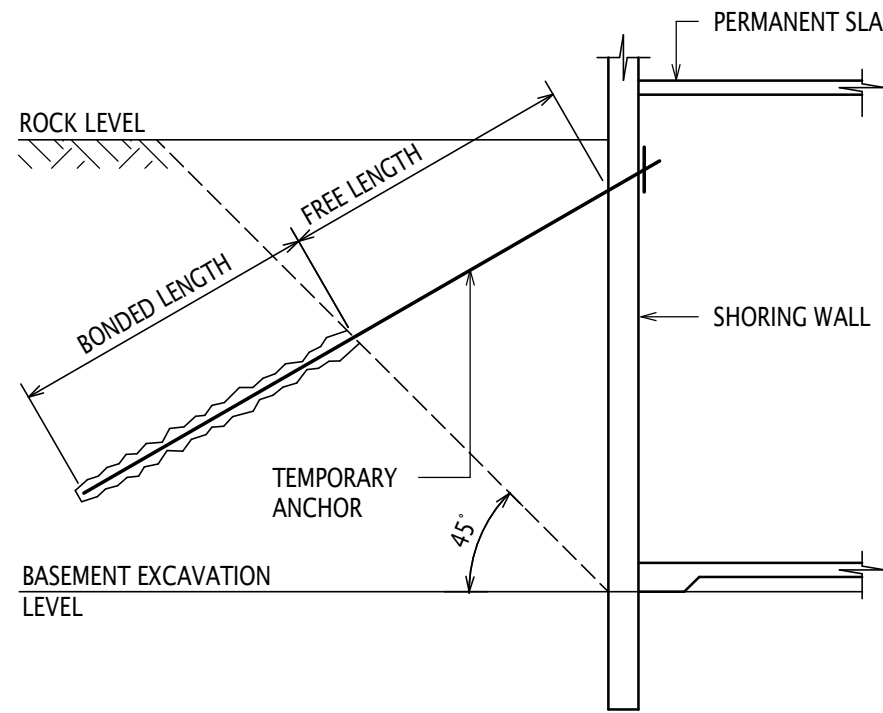
RBG-XX-XX-DR-SI-01311 P1



TYPICAL CONTIGUOUS OR SOLDIER PILE WITH ANCHOR
SCALE 1:20
READ IN CONJUNCTION WITH TYPICAL BORED PIER DETAILS & WALL ELEVATIONS

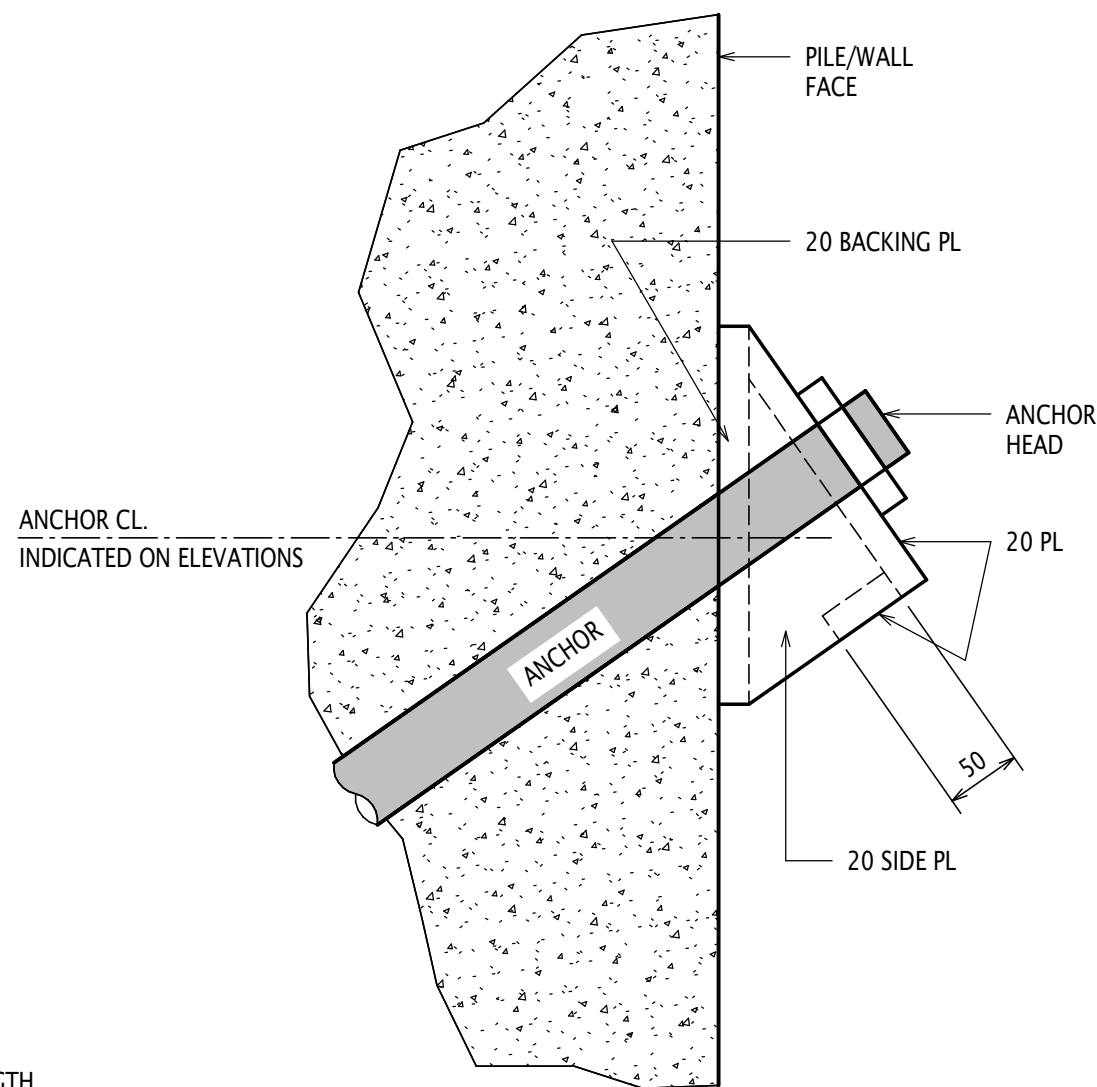


TYPICAL CONTIGUOUS OR SOLDIER PILE WITH WALLER
SCALE 1:20
READ IN CONJUNCTION WITH TYPICAL BORED PIER DETAILS & WALL ELEVATIONS

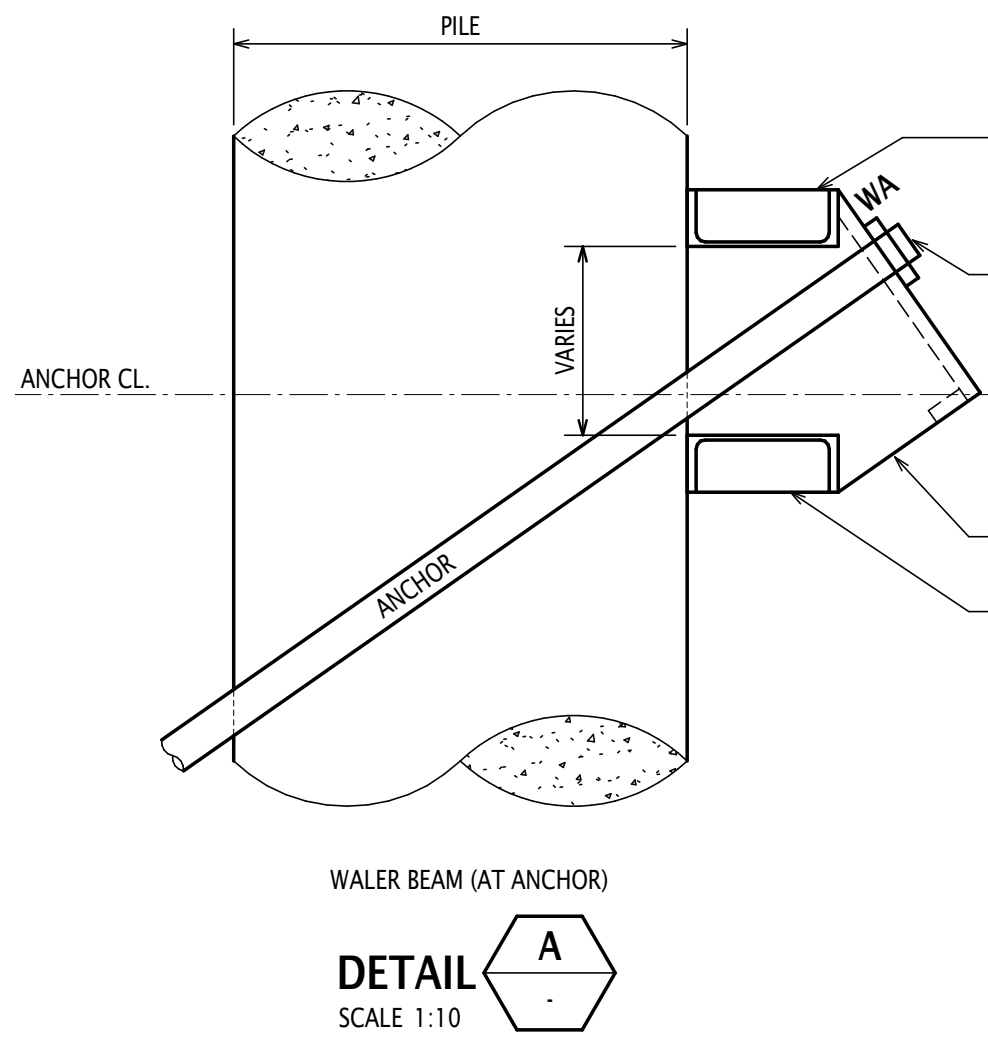


1. FREE LENGTH IS TO BE GROUTED AFTER ANCHOR IS STRESSED
2. REFER GEOTECHNICAL REPORT AND ADVICE FOR CALCULATION OF THE REQUIRED BONDED LENGTH
3. ALL BASEMENT ANCHORS TO BE DESTRESSED AFTER THE GROUND LEVEL SLAB CONNECTIONS HAVE BEEN GROUTED/POUR STRIPS HAVE BEEN CONSTRUCTED AND HAVE ACHIEVED DESIGN STRENGTH

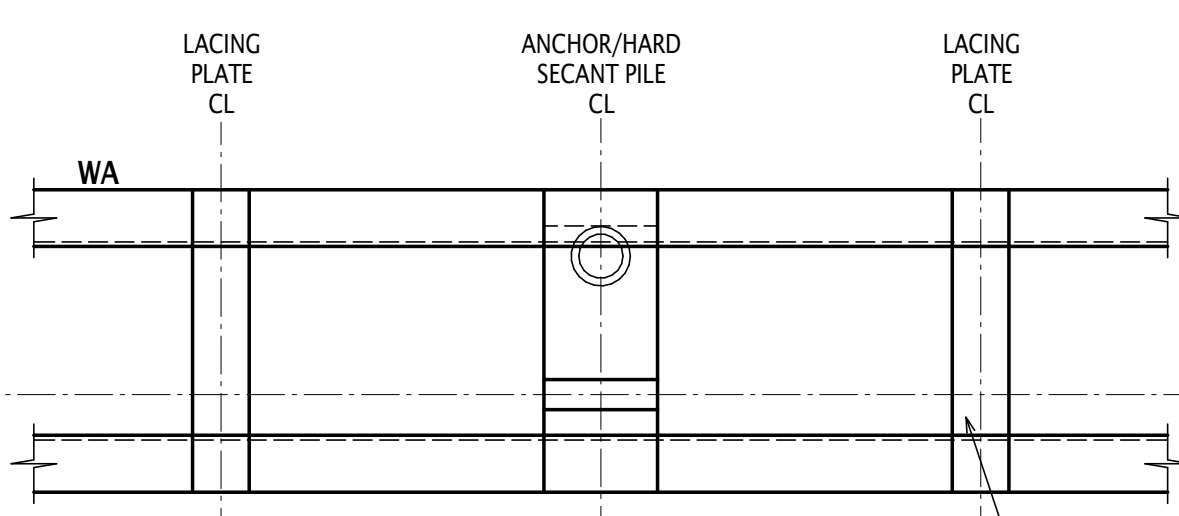
TYPICAL ANCHOR NOTES



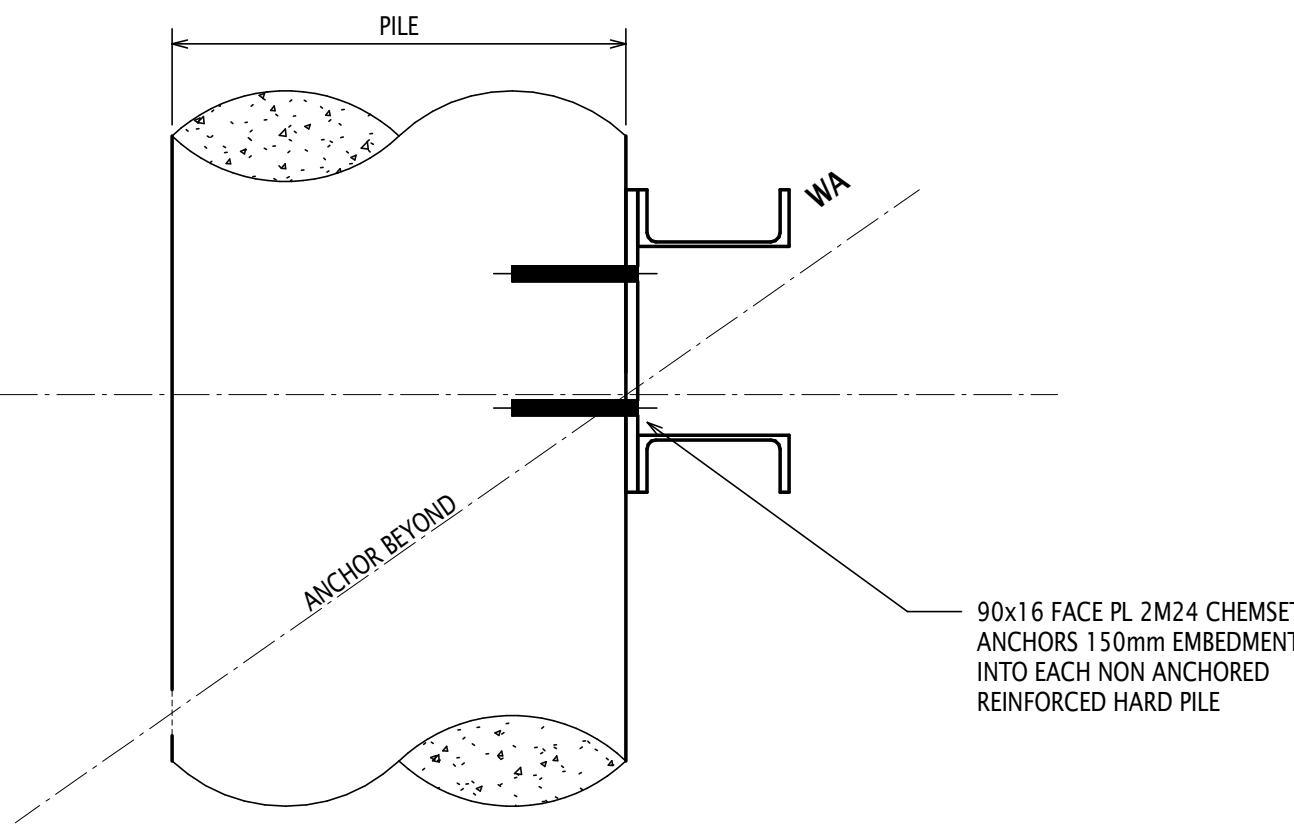
TYPICAL ANCHOR HEAD DETAIL
SCALE 1:10



WALLER BEAM (AT ANCHOR)
DETAIL A
SCALE 1:10



TYPICAL ANCHOR & WALLER BEAM ELEVATION
SCALE 1:10



WALLER BEAM (AT NON-ANCHOR)
DETAIL B
SCALE 1:10

P1 EARLY WORKS INFORMATION ONLY					ST	CA	25.11.19
Rev	Revision Description			By	App	Date	
1	1	1	1	1	1	1	
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DO NOT SCALE DRAWINGS. USE FIGURED DIMENSIONS

REFER TO GENERAL NOTES UNLESS NOTED OTHERWISE

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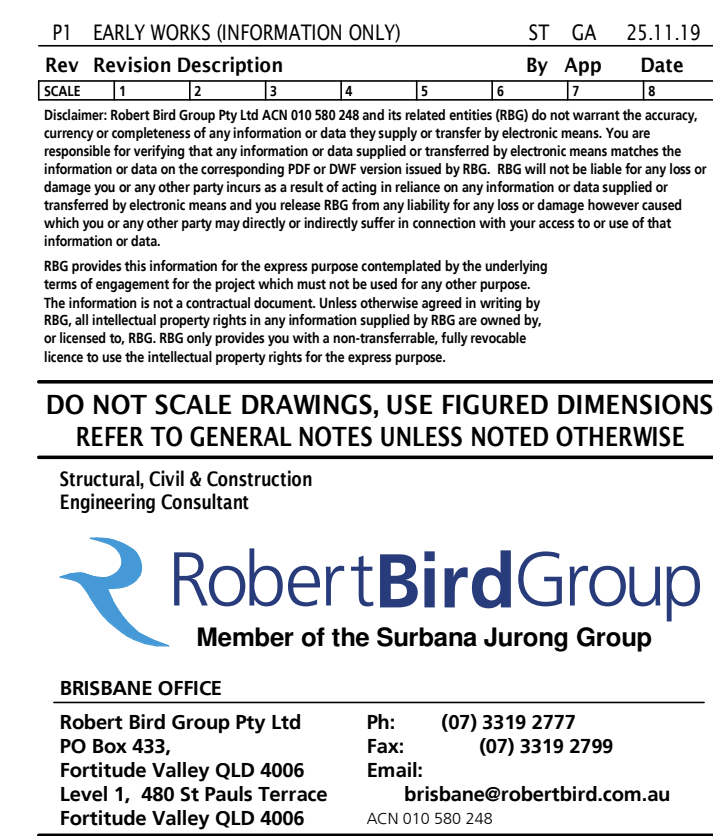
Client
BUILT PTY LTD

Project
LIVERPOOL CIVIC PLACE

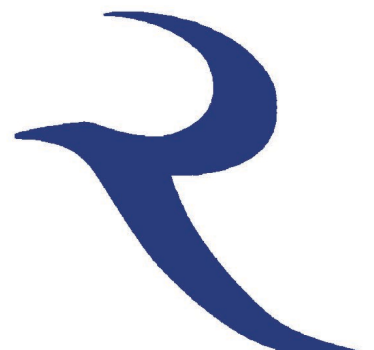
Title
**TYPICAL SHORING DETAILS
SHEET 2**

Date	Drawn
Scale at A0 1:1, 1:10, 1:20	Designer
Job Number 19280	Design Checker
Approved	Approved

NOT FOR CONSTRUCTION
Drawing Number
RBG-XX-XX-DR-ST-01312
Revision
P1



Drawing Number	Revision
RBG-XX-XX-DR-ST-01321	P1



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